TACAIR Material Readiness in Operation Allied Force

Peter J. Francis



4825 Mark Center Drive • Alexandria, Virginia 22311-1850

Copyright CNA Corporation/Scanned October 2002

Approved for distribution:

June 2001

al) Ma

Alan J. Marcus, Director Infrastructure and Readiness Team Resource Analysis Division

This document represents the best opinion of CNA at the time of issue. It does not necessarily represent the opinion of the Department of the Navy.

Approved for Public Release; Distribution Unlimited. Specific authority: N00014-00-D-0700. For copies of this document call: CNA Document Control and Distribution Section at 703-824-2123.

Copyright © 2001 The CNA Corporation

Contents

Introduction	1
Data	2
Down-after-sortie model	2
Downtime duration model	4
Summary and conclusions	5
Appendix A. Down-after-sortie model results	7
Appendix B. Downtime hazard model results	13
Bibliography	17
List of figures	19
List of tables	21

Introduction

This work was done as part of a larger study conducted for N814. The purpose of the larger study was to examine the link between mission performance and readiness drivers using data from CVN–71's combat operations during Operation Allied Force (OAF). In this part of the project, we looked specifically at material readiness of the embarked airwing (CVW–8).

Our original intent was to estimate the parameters for a complete Markov model of aircraft material condition. The transition matrix shown in figure 1 gives the general structure of such a model. Each aircraft was to be considered in one of three discrete states: airborne, not airborne but mission capable, or not mission capable. Transition probabilities between the states were to work as shown in figure 1. For example, p1 represents the probability that an aircraft that is not mission capable during one period would be in the same state during the next period.

Figure 1.	Transition matrix representing a Markov
	model of aircraft material condition

Time t		Time t+1	
	NMC	MC on board	In flight
NMC	р1	1 - p1	0
MC on board	р2	р3	1 - p2 - p3
In flight	р4	р5	1 [.] - p4 - p5

We were unable to implement a complete realization of this model because of problems that included missing data and resource constraints. However, we were able to make substantial progress on two components of the process in figure 1, and we present these results below.

Data

Data sources were our Maintenance Action Form (MAF) database for information on sorties and transitions between states for individual airframes, and ISIS data that allowed us to link pilots to particular sorties. Information on aircraft age (for F/A–18s) came separately from NAVAIR. For reasons that we do not understand, NALCOLMIS data for this battlegroup are not available for April of 1999; we are therefore limited to May and early June as the only periods of OAF for which we have data. Summary statistics are listed in table 1, and figure 2 shows how the sortie durations were distributed across squadrons and over time.

Table 1. Summary statistics

Number of sorties	814
F–14 sorties	48.8%
Training sorties	30.2%
Support sorties	3.2%
Percent down after sorties	25.3%
Average length of sorties	2.35 hours
Average pilot experience	935 hours
Average a/c age (F/A-18s only)	7.25 years
Average down spell after sortie	17.9 hours

Down-after-sortie model

The failure-after-sortie model corresponds to probability p4 in figure 1. We estimated a binary dependent variable (probit) model where the dependent variable was whether the aircraft went to a "down" status within one hour of completing a sortie. Full model results are in appendix A, but our principal conclusions are as follows:

• The type of flight mattered, with training and overhead flights being more likely to result in a subsequent down spell than operational flights. However, it isn't clear that this relationship is directly causal, at least for the training flights. Planes that were due to go



Sortie Lengths

Figure 2. Distribution of sortie duration across squadrons and over time

down later anyway might well be those that were designated for training activity. Also, most of the overhead flights were functional check flights that occurred immediately after a major overhaul or repair. Thus, it perhaps should come as no surprise that there is a greater-than-usual need for maintenance work after the check flight because some aspects of the overhaul may not have been done correctly.

• There were marked differences between squadrons, and again, it isn't clear how to interpret these differences. A greater

tendency to take a plane down may be due to more alert crews, but it could also be due to poor earlier work.

- Because aging platforms are an increasing source of concern for the Navy, we tried to identify age effects. At the time we did this work, we had age data for the F/A–18s in CVW–8 only. We estimated this same model for just those aircraft and included age as an independent variable. For F/A–18s, the model produced an estimate that an additional year of age increased the propensity to go down after a sortie by 3.6 percent. However, this result was not statistically significant.
- We included sortie length and pilot characteristics in the model, but neither of these had a statistically significant effect.
- We can get a rough indication of whether this type of model is a good fit by simply counting actual and predicted outcomes. When we did that here, we found that, for the full sample of sorties, there were ten observations (sorties) where the estimated probability of a plane going down was greater than 50 percent. In six of the ten sorties, the planes did in fact go down within an hour of landing.

Downtime duration model

The other portion of a Markov-type model that we examined was a duration (hazard) model of aircraft downtime. This would loosely correspond to estimating pl in figure 1. We estimated it using the data from the sortie database—that is, we used only those down spells that were attributed to sorties in the model of the previous section. Therefore, this model doesn't use down spells for aircraft that were taken down more than one hour after they returned from a flight, and, consequently, it doesn't fully reflect the effects of routine scheduled maintenance.

We present complete documentation (LIMDEP output) in appendix B, but this is a summary of the key results:

• In general, sortie-specific variables had little effect on downtime. The exception was if the sortie was for training: There was a statistically significant increase in downtime associated with sorties with a training flight purpose code. It isn't clear why this should be so, although our speculations concerning the selection of aircraft for training purposes may be appropriate here too.

- F-14s stayed down longer that F/A-18s. This is not surprising because the F/A-18 is well known for being relatively easy to work on.
- The age effect was again positive and not statistically significant.
- We chose the Weibull as the distribution for the hazard function because of its generality. (It allows for either an increasing or decreasing hazard function, and the constant-hazard special case is simply the exponential distribution.) From the actual model estimation, we can conclude that the downtime durations seem to follow a distribution that is significantly different from the exponential and has a decreasing hazard. This is consistent with previous CNA research on logistics system performance. (See [2].)

Summary and conclusions

We have identified some of the variables that would seem to be relevant to the determination of some of the transition probabilities for a Markov model of aircraft availability. These models can probably be refined even further. One important factor that was not allowed for was the length of time on station; this would likely have a deleterious effect on both people and machines. Characteristics of the individual maintainers was another factor that we could not incorporate due to data limitations. We hope to be able to match maintainer personnel data to MAFs in the future.

Note that there is a considerable similarity between the framework we are considering here and earlier work on sortie-generation models. (See [3, 4].) However, in those models, the probability distributions were seen as essentially fixed, whereas in this analysis, we are trying to allow for the possibility that some factors—"squawk rates," for example—can be expected to vary at least somewhat in response to factors that we can measure.

+ -

Appendix A. Down-after-sortie model results

We did all our statistical modeling with the LIMDEP econometric software package. Text output from the down-after-sortie model follows. We present results present for the entire CVW-8 fighter and attack population, and then for F/A-18s only. Most of the variables are self-explanatory, but two of them merit comment. FLTHRSQR, which is the square of flight hours, was introduced to accommodate possible nonlinearities in the relationship. SFTI refers to the rating system for pilots discussed in [5, pg. 56]. Hours refers to the number of hours the pilot had flown on the particular T/M/S.

I. Combined F-14s and F/A-18s

	+				· +·
	Binomial P:	robit Model			
	Maximum Li	kelihood Estimat	es		
	Dependent	variable	UPORD	OWN	
	Weighting	variable		ONE	
	Number of (observations		814	
	Iterations	completed		5	
	Log likeli	hood function	-416.9	280	
	Restricted	log likelihood	-460.4	669	1
	Chi-square	d	87.07	775	
	Degrees of	freedom		9	
	Significan	ce level	.0000	000	
	+				·+
+	-++		-++		++
Variable	Coefficient	Standard Error	b/St.Er.	P[Z >z]	Mean of X
+	-++		-++		++
_	Index function f	or probability			
Constant	-1.478689920	.48333903	-3.059	.0022	
VF14	.1788728074	.13695153	1.306	.1915	.26044226
VF41	3889974744E-01	.14187899	274	.7839	.22727273
VFA15	9651991829	.16151980	-5.976	.0000	.28992629
FLTHRS	.4181767389	.29599695	1.413	.1577	2.3484029
FLTHRSQR	5578390117E-01	.44413665E-01	-1.256	.2091	6.4334890
TRAINING	.3781438865	.14247535	2.654	.0080	.30221130
SUPPORT	.5890132056	.30143126	1.954	.0507	.31941032E-01
SFTI	.3169089817E-01	.57949122E-01	.547	.5845	3.0294840
HOURS	.1168902453E-03	.12453372E-03	.939	.3479	934.63857

(Note: E+nn or E-nn means multiply by 10 to + or -nn power.) +----+ | Partial derivatives of E[y] = F[*] with | | respect to the vector of characteristics. | They are computed at the means of the Xs. Observations used for means are All Obs. +--------+ Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X Index function for probability .14321719 -3.088 .0020 Constant -.4421851784 VF14 .5517223277E-01 .43501586E-01 1.268 .2047 .26044226 -.276 .7822 VF41 -.1153825076E-01 .41738818E-01 .22727273 VFA15 -.2415348880 .31440892E-01 -7.682 .0000 .28992629 .1250509341 .88455194E-01 1.414 .1574 FLTHRS 2.3484029 FLTHRSOR -.1668153272E-01 .13274642E-01 -1.257 .2089 6.4334890 .1189752113 .46683921E-01 2.549 .0108 TRAINING .30221130 SUPPORT .2067590720 .11701175 1.767 .0772 .31941032E-01 .9476797851E-02 .17327290E-01 .547 .5844 SFTI 3.0294840 .3495468067E-04 .37259672E-04 HOURS .938 .3482 934.63857 (Note: E+nn or E-nn means multiply by 10 to + or -nn power.) +--------+ | Fit Measures for Binomial Choice Model | Probit model for variable UPORDOWN +-----+ Proportions P0= .746929 P1= .253071 N = 814 NO= 608 N1= 206 | LogL = -416.92804 LogL 0 = -460.4669 |+-------+ Efron McFadden Ben./Lerman .09517 .09455 .65766 Cramer | Veall/Zim. | Rsqrd_ML .09454 .18205 .10145 Information Akaike I.C. Schwartz I.C. | Criteria 1.04896 900.87569 | +-----+ Frequencies of actual & predicted outcomes Predicted outcome has maximum probability. Threshold value for predicting Y=1 = .5000Predicted _____ + ____

Actual	0	1	Tota	1				
0 1	604 200	4 6	+ 60 20	- 8 6				
Total	804	10	+	4				
> Prob supp Normal e	oit; lh:	s=Upor om ite	down; r rations	hs=one,ao . Exit st	cage,vf catus=0	a15,Flthrs	s,flthrsg:	r, training,
II. F/A–1	8s only.							
	-	Bino Maxi Depe Weig Numb Iter Log Rest Chi- Degr Sign	mial Pr mum Lik ndent v hting v er of o ations likelih ricted squared ees of ificanc	obit Mode elihood F ariable ariable bservatic completed ood funct log like freedom e level	el Estimat ons d lion lihood	es UPORD -168.7 -193.4 49.31 .0000	OWN ONE 417 5 557 127 406 8 000	+
+ Variabl	.e Coe	effici	+- ent	Standard	Error	++ b/St.Er.	P[Z >z]	-++ Mean of X
Constan ACAGE VFA15 FLTHRS FLTHRSQ TRAININ SUPPORT SFTI HOURS	Index it -2 pr763 iG .908 178	func 2.4460 .15939 .97115 .44502 .43856 .18259 .68387 305477 397634	tion fo 23800 63571 41856 33708 94E-01 54579 44847 78E-01 17E-03	r probab: 1.5 .169 .177 .616 .122 .227 .450 .7212158 .180512	ility 340101 382052 341141 528718 148838 798726 383337 34E-01 10E-03	-1.595 .939 -5.600 .722 627 .801 1.517 1.259 991	.1108 .3479 .0000 .4702 .5308 .4232 .1293 .2080 .3214	7.2481439 .56594724 2.1491607 4.9658993 .33093525 .33573141E-01 2.8848921 847.77410

______ | Partial derivatives of E[y] = F[*] with | | respect to the vector of characteristics. | They are computed at the means of the Xs. Observations used for means are All Obs. +---------+ |Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X| Index function for probability -.5514477497 .34376591 Constant -1.604 .1087 ACAGE .3593536678E-01 .38330485E-01 .938 .3485 7.2481439 -.2338379454 .41770843E-01 -5.598 .0000 VFA15 .56594724 FLTHRS .1003290060 .13831590 .725 .4682 2.1491607 FLTHRSQR -.1716637367E-01 .27281959E-01 -.629 .5292 4.9658993 TRAINING .4253006984E-01 .54656587E-01 .778 .4365 .33093525 .2042692970 .16251556 1.257 .2088 .33573141E-01 SUPPORT SFTI .2047178624E-01 .16265249E-01 1.259 .2082 2.8848921 -.4034960776E-04 .40713239E-04 -.991 847.77410 HOURS .3217 (Note: E+nn or E-nn means multiply by 10 to + or -nn power.) +--------+ Fit Measures for Binomial Choice Model | Probit model for variable UPORDOWN +------+ Proportions P0= .824940 P1= .175060 417 NO= 344 N1= 73 N ≈ LogL = -168.75566 LogL0 = -193.4127 +------+ Efron McFadden Ben./Lerman .11871 .12748 | .74516 Cramer | Veall/Zim. | Rsqrd_ML .11779 .21976 .11153 +----+ | Information Akaike I.C. Schwartz I.C. | Criteria .85255 391.80909 +----+ Frequencies of actual & predicted outcomes Predicted outcome has maximum probability. Threshold value for predicting Y=1 = .5000Predicted ----- + -----

Appendix

Actual	0	1		Total
			+	
0	343	1		344
1	72	1		73
		·	+	
Total	415	2		417

Appendix B. Downtime hazard model results

Here we give the text output for the downtime hazard model. As in appendix A, we present combined F–14 and F/A–18 results first, followed by separate results for F/A–18s only. Note that it is necessary to take the natural logarithm of downtime for use in this routine. The "sigma" in this output is the parameter that determines the slope of the hazard; the fact that it is significantly different from one in the first regression establishes that the hazard function in that case is not exponential. (It is borderline significant in the second regression.)

I. Combined results for F-14s and F/A-18s

	+				+
	Loglinear sur	vival model:	WEIBULL		
	Maximum Like]	ihood Estimat	es		
	Dependent var	riable	LNDW	NTIM	
	Weighting var	riable		ONE	
	Number of obs	servations		208	
	Iterations co	ompleted		14	
	Log likelihoo	d function	-417.	9449	
	+				-+
+ Variable +	+++ Coefficient St ++	andard Error	+ b/St.Er. +	+	++] Mean of X ++
1	RHS of hazard model	L			
Constant	2.496620695	1.0964933	2.277	.0228	
VF14	-1.659409229	.34949381	-4.748	.0000	.42788462
VF41	6713862412	.33514312	-2.003	.0451	.28846154
VFA15	-1.110724834	.87002803	-1.277	.2017	.43269231E-01
FLTHRS	.7252487158	.70132916	1.034	.3011	2.4639423
FLTHRSQR	1399716072	.10076648	-1.389	.1648	7.3610096
TRAINING	8916738957	.31887733	-2.796	.0052	.35096154
SUPPORT	2672918828	.54106707	494	.6213	.52884615E-01

```
Ancillary parameters for survival
        1.691159392 .97149294E-01 17.408 .0000
Sigma
(Note: E+nn or E-nn means multiply by 10 to + or -nn power.)
    Parameters of underlying density at data means:
  Parameter Estimate Std. Error Confidence Interval
  .0955 to
                   .02211
  | Lambda
           .13884
                                      .1822
                    .03397
  | P
            .59131
                            .5247 to
                                      .6579
  Median 3.87515 .61717 2.6655 to 5.0848
  Percentiles of survival distribution:
          .25
  Survival
                 .50 .75
                               .95
                  3.88
           12.51
                         .88
  Time
                               .05
  --> Reject; age < 0 $
--> Survival; lhs=LnDwnTim;
  rhs=one,age,vfa15,Flthrs,flthrsqr, training, support;
  model=Weibull $
Normal exit from iterations. Exit status=0.
II. Results for F/A–18s only
         +------------+
         | Loglinear survival model: WEIBULL
         Maximum Likelihood Estimates
                        LNDWNTIM
         | Dependent variable
                              ONE
         Weighting variable
                                 59
         Number of observations
         Iterations completed
                                 14
         Log likelihood function
                             -108.6682
```

Appendix

|Variable | Coefficient | Standard Error |b/St.Er.|P[|Z|>z] | Mean of X| +----+----+ RHS of hazard model Constant .7007576221 4.8927149 .143 .8861 AGE .5270809643 .39845108 1.323 .1859 7.3998805 VFA15 .65406279 -1.456 .1455 -.9520432114 .15254237 3.1695339 -.074 .9408 FLTHRS -.2352836102 2.0474576 FLTHRSQR -.5385881816E-01 .76223681 -.071 .9437 4.5077965 FLTHKSQR-.5385881816E-01.76223681-.071.94374.5077965TRAINING-1.545007594.78947811-1.957.0503.40677966 SUPPORT -2.793202177 1.5556986 -1.795 .0726 .84745763E-01 Ancillary parameters for survival Sigma 1.302560425 .16626092 7.834 .0000 (Note: E+nn or E-nn means multiply by 10 to + or -nn power.) Parameters of underlying density at data means: Parameter Estimate Std. Error Confidence Interval .05692 Lambda .01085 .0357 to .0782 .76772 .5757 to .09799 P .9598 | Median 10.89991 2.07784 6.8273 to 14.9725 Percentiles of survival distribution: Survival .25 .50 .75 .95 Time 26.89 10.90 3.47 .37

.

.

Bibliography

- [1]Peter Francis and Geoffrey Shaw. Effect of Aircraft Age on Maintenance Costs, March 2000(CNA Annotated Briefing D0000289.A2)
- [2] Walter R. Nunn and Ronald H. Nickel. Part Replacement Time Analysis, Apr 2000 (CNA Research Memorandum D0000743.A1)
- [3] Walter R. Nunn. A Simple Monte Carlo Sortie-Generation Model for Carrier Aircraft, Apr 1986 (CNA Research Contribution 542)
- [4] Walter R. Nunn. A Visual Basic Version of the Sortie-Generation Model Muir3, June 1996 (CNA Research Memorandum 96–85)
- [5] Laura J. Junor et al. Trends in Interdeployment Training Readiness: A Study of the Bathtub, Oct 2000 (CNA Research Memorandum D0002077.A2)

List of figures

Figure 1.	Transition matrix representing a Markov model of aircraft material condition	1
Figure 2.	Distribution of sortie duration across squadrons and over time	3

.

List of tables

Table 1. Summary statistics	Ž
-----------------------------	---